MULTIBODY DYNAMIC ANALYSIS
AND SIMULATION OF ENGINE
MODEL

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Abstract
An assembly model for the internal combustion engine model has been proposed. The basis for the model is a
study of earlier designs. The proposed design will run at a different speed, so the designers want to analyse the
components, and in particular the stress in the connecting-rod, at the new speed.

The designer's question is: at what speed can the engine be run without the stress in the connecting rod
exceeding the permissible stress for the material?

Keywords: Multibody Dynamic Simulation, Finite Element Analysis, HyperWorks, Engine Model

Introduction
In the last years finite element analysis has evolved as a powerful tool for supporting engineers in various fields
of product development and research with the continuous increasing computational capabilities . These technique
become more and more important for the effective development of competitive products.

IC (Internal Combustion) engines have been around for more than a century now and do not seem to be
replaceable – not by any means completely - in the foreseeable future. The four-stroke variety is more
commonly used as the source of motive power for applications such as automobiles. The performance of such
an engine in terms of power, emissions and cost has changed drastically, from the time it was invented, though
the basic governing thermodynamic cycle remains more or less the same. The four-stroke IC engine needs
constant refinement as emission targets, which a vehicle must meet, become increasingly challenging. In
addition, there is an ever-increasing demand on efficiency for which the need may be to step-up power-to-
weight ratio of an engine as much as possible. Automotive companies bear huge cost in honing and updating IC
engine technologies to meet some of the challenges mentioned. The advancement in computational techniques
has greatly contributed to these efforts by offering opportunities for multiple design options to be evaluated
virtually there by saving a great deal of investments associated with building of multiple prototypes.

The current project describes a semi-integrated CAE (Computer-Aided Engineering)-Based approach for the
assessment of a reciprocating Internal Combustion (IC) engine design with single cylinder which is a complex
multi-scale, multi-physics system with high non-linearity between the interacting components. The current
practice in industry is to follow a piecemeal approach in which considerations of combustion, structural
vibration and acoustics, fluid dynamics, thermal management, etc. are attended separately in the performance
evaluation and optimization of an engine configuration representing key components such as pistons, connecting
rods, and crankshaft, cylinder head and cylinder liners. A major difficulty in realizing a fully-integrated detailed
analysis of an engine is the complex interactions between the domains mentioned. Consequently, at present, only simplified and semi-empirical tools based on lumped parameter modelling are available for modelling the multi-disciplinary behaviour of an IC engine system. With the advancement in CAE tools, it becomes easy to improve computational efficiency and to check practicability of design optimization.

The simulation methodology studied here is based on explicit dynamic finite element analysis using a commercial code in which contacts between relevant parts transferring motion are accounted for in the analysis. Crankshaft is a large component with a complex geometry in the engine, which converts the reciprocating displacement of the piston to a rotary motion with a four link mechanism. This study was conducted on a single cylinder four stroke cycle engine. Rotation output of an engine is a practical and applicable input to other devices since the linear displacement of an engine is not a smooth output as the displacement is caused by the combustion of gas in the combustion chamber. A crankshaft changes these sudden displacements to a smooth rotary output which is the input to many devices such as generators, pumps, compressors, etc.

This problem involves more than just an "FEA for stress analysis". In many situations, forces and restraints are not supplied. The designer has to estimate these and then perform the stress-analysis. This subject shows how to use OptiStruct / Analysis to integrate these two tasks. The components move as a mechanism - they make up a 4 bar mechanism with four joints.

Table: 1

<table>
<thead>
<tr>
<th>Bar No.</th>
<th>Bar Name</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Crankshaft</td>
</tr>
<tr>
<td>2</td>
<td>Connecting Rod</td>
</tr>
<tr>
<td>3</td>
<td>Piston</td>
</tr>
<tr>
<td>4</td>
<td>Cylinder and Block (Ground)</td>
</tr>
</tbody>
</table>

Steel
- $E: 2.07 \times 10^{11} \text{N/m}^2$
- $v: 0.3$
- $\rho: 7.83 \times 10^3 \text{Kg/m}^3$
### Joints Between Elements

<table>
<thead>
<tr>
<th></th>
<th>Motion</th>
</tr>
</thead>
<tbody>
<tr>
<td>Crankshaft and Block</td>
<td>Revolution</td>
</tr>
<tr>
<td>Crankshaft and Connecting Rod</td>
<td>Revolution</td>
</tr>
<tr>
<td>Connecting Rod and Piston</td>
<td>Revolution</td>
</tr>
<tr>
<td>Piston and Cylinder</td>
<td>Translation</td>
</tr>
</tbody>
</table>

So the first task is to calculate the forces in the components as the engine reciprocates. These forces should then be used to calculate the dynamic stresses in the component of interest - the connecting rod. It is important that one realizes that the first task involves a rigid-body analysis, while the second involves a flexible-body analysis. The approach taken in this project makes use of the capability of OptiStruct / Analysis to mix both forms of analysis using component-mode synthesis.

The project explores the use of "bodies" and "joints" together with "elements" that the FE analyst is more familiar with.

### Background

The project spans two separate branches of mechanics: continuum mechanics for stress analysis, and rigid body dynamics for calculation of forces.

The latter does not require 3D geometry, since the mass and inertial properties are adequate. However the availability of the 3D geometry makes it much easier to understand the results of the analysis. In addition, the use of the component mode synthesis approach means that the “flexibility” as calculated by the finite element method can be used to calculate dynamic stresses easily.

To appreciate the convenience of the method, it is interesting to contrast it with a "traditional" analysis. This would require that:

- the properties be calculated using a 3D model, typically a CAD model
- these properties be transferred to a motion-simulation tool that can perform "dynamic" analysis, not simple "kinematic" analysis
- the dynamic simulation be carried out and forces obtained as output
- forces be transferred to a Finite Element model
- the stress analysis be performed using the Finite Element model

With the integrated approach, the various "transfers" of data are eliminated, not only making the process easier and faster but also reducing scope for error.

Not only can forces be output and graphed, the stresses can be calculated automatically and displayed on the animation of the components.

### Planning and Organization

Most FE models contain a lot of data. There is the geometry (usually received from CAD) and the elements, restraints and loads. There is also some data that cannot be depicted graphically, such as the Modulus of Elasticity.

Planning how to organize this data goes a long way towards making the model easy to use.

HyperMesh uses collectors to organize entities - that is, geometry, elements, loads, restraints and materials. Our model will have one material (Steel), and several components for elements even though all will be modelled with solid elements. We will follow this approach since it makes it easier to define "bodies" for the mechanisms analysis.
The geometric entities (lines, surfaces, solids, points) are of no relevance to the FE solver. They are important only to help define the elements. The elements themselves, however, inherit some properties from the collector they are in - most important for us is the material data. We will ensure that the elements are in a collector that has been assigned the correct material.

We can also neglect some details in the geometry. This phase is called Geometry Clean-up. We will use this for convenience, rather than to control CPU-time and accuracy, since our focus is on setting up the multi-body problem, not on generating a high-quality mesh.

To sum up, our model will contain:

- one material collector
- several collectors for elements
- several collectors for solution-control

There may be other collectors which are not important for the FE solution. They will be used for convenience as and when required.

**Multi-Body-Dynamics (MBD) Modelling**

The modelling focus is on creation of joints and bodies.

OptiStruct / Analysis require that the two grids be used to define revolute and translational joints - one grid on each of the bodies. The grids that define the joints need to be on the axis of rotation, for a revolute joint. Since there may not be elements at the desired location, we make liberal use of "rigid" elements. These are equations that tell the solver that all "slave" nodes must move exactly as the "master" does. This approach allows us to define the grids for the joints at locations that are correct from the point of view of the multi-body solver.

Also, to ease visualization, we choose to create the joints with the grids in physically different locations. This way we can see the joint-definitions clearly. Once we have completed defining the joints, we move the grids and the associated bodies so that the "coincident grids" requirement is satisfied.

**Loads and Restraints**

This step is different from that of a "usual" Finite Element Analysis.

The use of "ground" bodies means we do not need any restraints on the FEA model. That is, we do not need any SPCs. Since this is a dynamic analysis, we will provide an initial velocity to the piston, to simulate the effect of a "kick-start".

Further, we define the interval for which we want to solve the problem. Note that unlike an FEA solution, the time-integration scheme used by the MBD solver embedded in OptiStruct / Analysis calculates the step-size for time-integration internally. Here, we specify the time-steps at which we want results reported.

This data is all that is required to generate the results.

**Running OptiStruct/Analysis**

Remember that the CPU time for analysis is an important criterion in any FEA. For a model that is finer than the one shown in the example, you may want to increase the RAM used. The on-line documentation explains how to do this.

One should be encouraged to treat computing resources as a valuable resource. In most engineering designs, quick results that are approximate are usually more valuable than more accurate results that take too long to deliver!
**Result and Analysis**

The multi-body dynamic analysis of the engine is carried out on the computer equipped with 3GB RAM and an Intel Core 2 duo processor for approximately one hour of engine running.

**Displacement**

The contour plot of displacement shows displacement of various element of the model engine from their initial positions. The red colour is used for showing maximum displacement while blue portion shows minimum displacement. The maximum displacement comes out to be $4.496 \times 10^2$ mm and minimum displacement is zero i.e. the centre axis of the crankshaft. The maximum displacement occurs in the crank and lower part of the connecting rod.

![Contour plot of displacement](image)

**Figure 2: Contour plot of displacement.**

**Stress**

Dynamic analysis of the engine model results in more realistic stresses whereas static analysis provides overestimated results.

The stresses in the engine components are generated due to inertia and the combustion of the fuel. These two load sources cause both bending and torsional load on the crankshaft, bending on connecting rod, compressive load on piston, etc. The initial starter velocity to the piston is given 4mm/s and it is seen that after this starter velocity the engine starts running and the stress comes out to be zero. It means that this the starter velocity at which engine runs is stress free. Beyond this velocity if engine runs, the stresses will be generated in the engine components.
Figure 3: Contour plot of stress free motion.
Output files

The various output files are generated after running the analysis.

<table>
<thead>
<tr>
<th>File Name</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>engine_frames.html</td>
<td>HTML report of the analysis, giving a summary of the problem formulation and the results from the final iteration.</td>
</tr>
<tr>
<td>engine.out</td>
<td>RADIOSS output file containing specific information on the file set up, estimates for the amount of RAM and disk space required for the run, and compute time information. Review this file for warnings and errors.</td>
</tr>
<tr>
<td>engine.h3d</td>
<td>Binary results file (Nodal results).</td>
</tr>
<tr>
<td>engine.stat</td>
<td>Summary of analysis process, providing CPU information for each step during analysis process.</td>
</tr>
<tr>
<td>engine_mbd.abf</td>
<td>Binary plotting file.</td>
</tr>
<tr>
<td>engine_mbd.h3d</td>
<td>Binary results file (Modal results).</td>
</tr>
<tr>
<td>engine_mbd.log</td>
<td>Log file from OS-Motion containing the information on the joints and markers, simulation etc., which are specific to MBD analysis.</td>
</tr>
<tr>
<td>engine_mbd.mrf</td>
<td>Binary results file for plotting.</td>
</tr>
<tr>
<td>engine_mbd.xml</td>
<td>Model file in .xml format – solver intermediate input deck.</td>
</tr>
</tbody>
</table>

Table3: The generated output file after running analysis.
Animations of motion are the classic output from a simple kinematic analysis. The first use of such an animation is simple a visual evaluation of motion for the designer to see if it is what is desired. More sophisticated animations can be created to show motion from critical angles or even looking inside of parts, which gives simulation a definite edge over building and running a physical prototype.

View the Results in HyperView

The results are viewed in HyperView module of HyperWorks which is launched from within the RADIOSS panel of HyperMesh.

HyperView is a complete post-processing and visualization environment for finite element analysis (FEA), multi-body system simulation, video and engineering data. The contour plot for displacement of engine components from their initial position and stresses in several elements are easily viewed. The engine.h3d file which is a binary result file (nodal result), is used for viewing the results. This file is fine to use because the .h3d format contains both model and result.

Conclusions

This project investigated design and FE analysis of engine critical components from the base design of in house exiting engine. The cost advantage of exiting proven design is used instead of going for a new development process. First of all the critical parts are digitized by 3D modelling software. Stress analysis was performed based on the input from proposed engine performance data, which comprised power output, crank, piston assembly.

The boundary condition of connecting rod and crankshaft are applied over the respective FE models which was created by using hyper mesh and the processing part was done by OptiStruct.

The result was viewed on HyperView. The contour plot for stress and displacement was plotted. The different input velocities were taken at trial and error method. The contour plot for stress shows that there is no stress developed in any component of the engine at a particular given speed of 4mm/s. So the model is successful for that speed or less. Beyond this the stresses will develop and the model will fail.

In case of cylinder block, the pre-processing part was finished and the boundary conditions are identified, the FE analysis part will be carried out later. The FE result is interpreted with the yield strength of thee component material and FOS was calculated. The outcome of this analysis predicts the safer working of the parts under the stated operating condition.

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References


